

Course Code	Course Title					Core / Elective	
PC402EE	ELECTRICAL MACHINES - I					Core	
Prerequisite	Contact Hours per Week				CIE	SEE	Credits
	L	T	D	P			
NIL	3	1	-	-	30	70	3

Course Objectives

- To learn and understand electromechanical energy conversion devices.
- To be able to understand in detail about DC machines. Construction, principle, performance characteristics and testing.

Course Outcomes

- Understand construction, operating principle and characteristics of different types of DC motors and generators
- Test and calculate performance parameters of DC motors and generators
- Select appropriate DC machines for a specific application

UNIT I

Electromechanical energy conversion: Principle of energy conversion, Flow of energy in electromechanical devices, Coupling-field reaction, Singly excited magnetic system – Electric energy input, Magnetic field energy stored, Mechanical work done – with slow, instantaneous and transient movement of armature, Calculation of mechanical force, Doubly excited magnetic systems, electromagnetic and reluctance torques.

UNIT II

DC Machines: Simple loop generator, Essential parts of DC machine, Details of Lap winding & Wave winding, EMF equation, Armature reaction — Remedies, Ampere turns, Commutation — reactance voltage, Methods of improving commutation — High resistance brushes, shifting of brushes, Interpoles, Compensating winding.

UNIT III

DC Generators; Classification & types of DC generators, Open circuit, Internal & External characteristics — Critical resistance & critical speed, Voltage regulation, Conditions for self excitation, Causes of failure of voltage buildup, Parallel operation Series, Shunt and Compound generators, Applications.

UNIT IV

DC Motors: Classification & Types of DC motors, Back emf, Speed regulation, Armature torque, Armature reaction, Operating characteristics, Performance curves, Basic speed control methods Shunt and Series motors, Three & four-point starters, Calculation of step resistances, Applications.

UNIT V

Testing, Losses and Efficiency: Power losses — Copper losses and Rotational losses, Power flow, Efficiency, Testing - Brake Test and Swinburne's test, Hopkinson's test, Field's test, Retardation test, Heat run test.

Suggested Reading:

1. D.P. Kothari, I.J. Nagrath, **Electric Machines**, Tata McGraw Hill, 4th Edition, 2010
2. Bhimbra P.S., **Electrical Machinery**, Khanna Publications, 2000
3. Gupta J.B., **Theory and Performance of Electrical Machines**, S.K. Kataria & Sons, Delhi, 2005.
4. AE Clayton and NN Hancock, **The Performance and Design of Direct Current Machines**, 3rd edition, 1959.

Electromechanical Energy Conversion

1. Principles of Energy Conversion
2. Flow of energy in electromechanical Devices
3. Coupling Field reaction
4. Singly excited Magnetic System
Electrical energy input - Magnetic field
Energy stored - Mechanical work done
with slow, instantaneous and transient
movement of armature
5. Doubly excited magnetic system,
electromagnetic torque
Reluctance torque.

Basis

a) Magnetic field → the space around the poles of a magnet in which the effect of magnetic force is felt.

b) the invisible lines of force surrounding the magnet is called the magnetic flux.

c) the force of attraction or repulsion, exerted by one magnet on the other is the magnetic force.

d) Coulomb's law → $F \propto \frac{m_1 m_2}{d^2}$ $m_1, m_2 \rightarrow$ pole strength
 $d =$ distance of separation

or $F = \frac{m_1 m_2}{4\pi \mu_0 \mu_r d^2}$ N.

m_1, m_2 in webers.
 d in meters.
 F in Newtons

e) Relative permeability μ_r
 the ratio of force of attraction or repulsion, between two poles m_1 & m_2 placed at a distance 'd' in a ~~medium~~ air and μ_r relative permeability μ_r and to that of force at same distance of separation, in air.

$F_{air} = \frac{m_1 m_2}{4\pi \mu_0 d^2}$ in Medium $F_{\mu_r} = \frac{m_1 m_2}{4\pi \mu_0 \mu_r d^2}$

$\mu_r = \frac{F_{air}}{F_{medium}}$

f) magnetic field strength :-

Force experienced per unit strength is magnetic field intensity.

$$F = \frac{m_1 m_2}{4\pi \mu_0 \mu_r d^2}$$

$$H = \frac{F}{m_1} = \frac{m_2}{4\pi \mu_0 \mu_r d^2} \quad \text{Where } m_1 = 1 \text{ and } m_2 = m.$$

then $H = \frac{m}{4\pi \mu_0 \mu_r d^2} \text{ N/Wb.}$

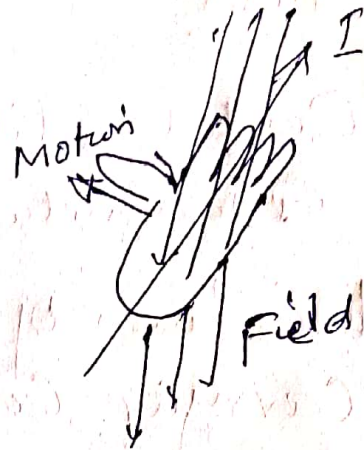
g) magnetic flux density $B = \frac{\Phi (\text{Wb})}{a. (\text{m}^2)}$ Scalar quantity
 $1 \text{ Wb/m}^2 = 1 \text{ Tesla.}$

h) B and H are directly proportional (assumption)
 $B = \mu_0 H.$ $\mu_0 =$ Permittivity of free space
 $= 4\pi \times 10^{-7}$

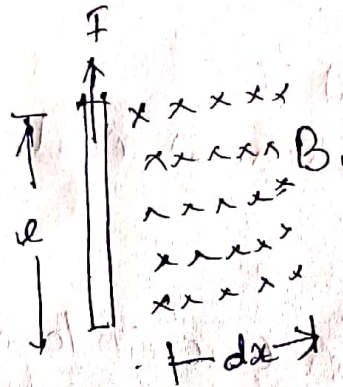
(d) Force on a current carrying conductor, in a magnetic field.

$$F = B I l \text{ since } N.$$

Fleming's left hand rule



m) Force on a conductor of length l carrying current I , in a field of flux density B .



$$F = B I l \text{ N.}$$

If work is done by moving the conductor against the force over a distance dx

$$\text{the work} = F \times dx = B I l \times dx$$

$$= B I (l \times dx) \text{ Joules} = B I \phi \text{ Joules}$$

Since $l \times dx = A$
and $B \cdot A = \phi$.

i) Current Carrying Conductor & Magnetic Field.

Oersted discovered the effect of current on a magnetic field.

The lines of force encircle a current carrying conductor and their direction is given by —

- (i) Cork screw rule, (ii) Right hand rule
- (iii)

(d) Ampere's circuit law: The magnetic field intensity vector H when summed up on a current carrying surface, gives the current enclosed.

$$\oint H \cdot dl = I$$

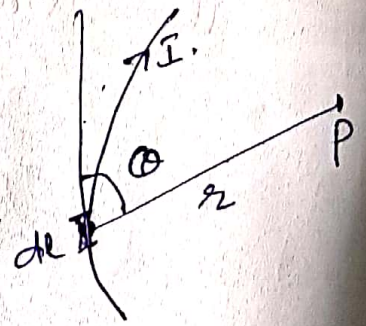
k) Biot-Savart's law.

Flux density dB at a point P , at a distance ' r ' from the element dl carrying current I is

Given by $dB \propto \frac{I dl \sin \theta}{r^2}$

or $dB = k \frac{I dl \sin \theta}{r^2}$

$$k = \frac{\mu_0 \mu_r}{4\pi}$$



(ii) Magnetostriction. The change in dimensions of the magnetic material, in the direction of magnetic field, is either expanding or contracting, of the order of 10^{-6} is called magnetostriction.

Magnetic Circuits → the closed path followed by magnetic flux is called the magnetic circuit.

Magneto motive force 'mmf' → the product of No of turns N and the current I flowing through it is called mmf. $MMF = \frac{NI}{\text{ampere turn}}$

Reluctance 'S' in a magnetic circuit is analogous to Resistance in electric circuit.

$$S = \frac{l}{\mu a} \quad \text{amp-turn/wb.}$$

Similar to Current I , flux in a magnetic circuit

$$\phi = \frac{\text{mmf}}{S} = \frac{AT}{l/\mu a} = \frac{AT}{l/\mu_0 \mu_r a}$$

$$AT = \frac{\phi \cdot l}{\mu_0 \mu_r a} = \left(\frac{\phi}{a}\right) \cdot \frac{l}{\mu_0 \mu_r} = \frac{B \cdot l}{\mu_0 \mu_r} = H \cdot l = \text{amp turn}$$

21) Magnetic material

a) Para magnetic material relative permeability > 1 having a small positive eg: Aluminium, tin, manganese

b) Diamagnetic material ; relative permeability less than 1. eg Bismuth, Copper,

c) Ferromagnetic material. very high relative permeability. eg: Iron, Cobalt, Nickel.

(i) Soft ferromagnetic \rightarrow easily magnetized and demagnetized

(ii) Hard ferromagnetic \rightarrow difficult to magnetize and demagnetize

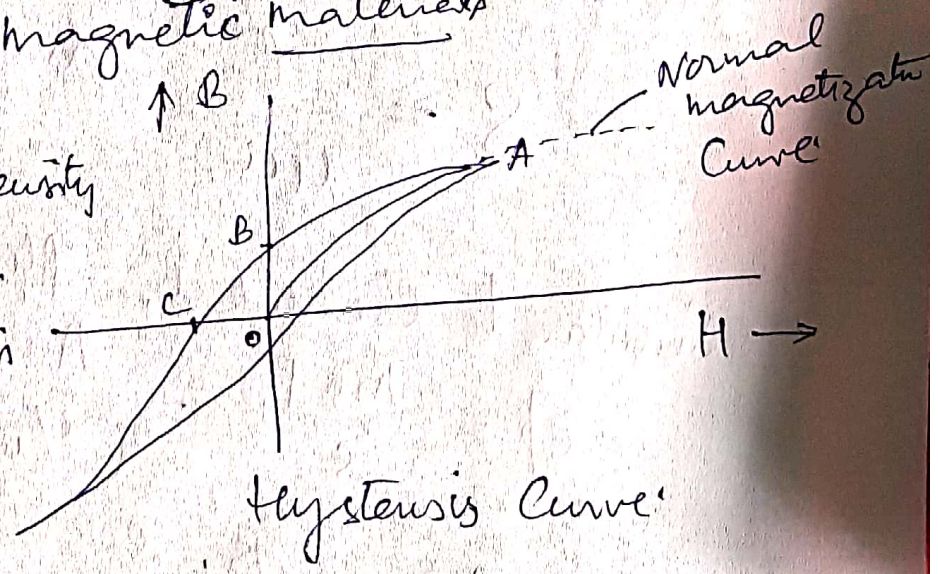
d) Ferrites \rightarrow intermediate to ferromagnetic and non magnetic material.

(i) Soft ferrites (ii) Hard ferrites

22) Properties of magnetic materials

(i) $OB =$ Residual flux density

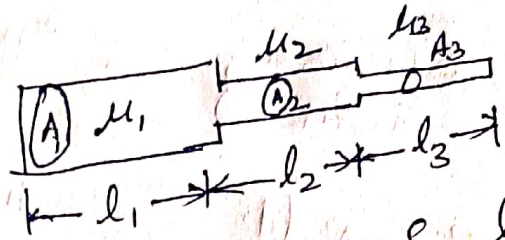
(ii) $OC =$ Coercive force for demagnetization



Composite magnetic circuit

$$S_2 = \frac{l_2}{\mu_0 \mu_2 A_2}$$

Total reluctance
 $S = S_1 + S_2 + S_3$



$$S_1 = \frac{l_1}{\mu_0 \mu_1 A_1}$$

$$S_3 = \frac{l_3}{\mu_0 \mu_3 A_3}$$

Total mmf = $\Phi \cdot S$

$$= \Phi (S_1 + S_2 + S_3)$$

$$= \Phi \left(\frac{l_1}{\mu_0 \mu_1 A_1} + \frac{l_2}{\mu_0 \mu_2 A_2} + \frac{l_3}{\mu_0 \mu_3 A_3} \right)$$

$$= \left(\frac{\Phi}{A_1} \right) \cdot \frac{l_1}{\mu_0 \mu_1} + \left(\frac{\Phi}{A_2} \right) \frac{l_2}{\mu_0 \mu_2} + \left(\frac{\Phi}{A_3} \right) \frac{l_3}{\mu_0 \mu_3}$$

$$= \left(\frac{B_1}{\mu_0 \mu_1} \right) l_1 + \left(\frac{B_2}{\mu_0 \mu_2} \right) l_2 + \left(\frac{B_3}{\mu_0 \mu_3} \right) l_3$$

$$= H_1 \cdot l_1 + H_2 \cdot l_2 + H_3 \cdot l_3$$

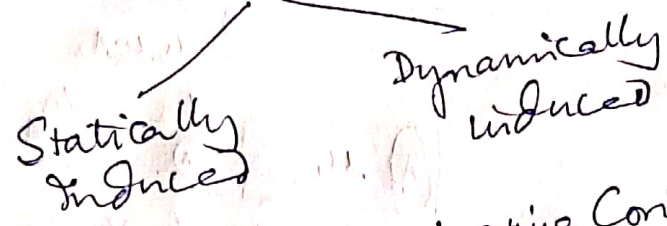
i.e. Total mmf = Sum of ampere turns of each part.

Magnetic leakage \rightarrow $\frac{\text{Total Flux}}{\text{Useful Flux}}$

leakage factor = $\frac{\text{Flux in iron path}}{\text{flux in air gap}}$

Flux in air gap = useful flux \rightarrow used for various applications

Induced emf.



$$e = -N \frac{d\phi}{dt}$$

Moving Conductor in a magnetic field

$$e = Blv \text{ Since Volts.}$$

Direction of Dynamically induced emf by Fleming's Right hand Rule

Self induced EMF

Mutually Induced EMF

$$e = -N \frac{d\phi}{dt} = -N \frac{d}{dt} \left(\frac{Ni}{\mu/\mu_0 \mu_r a} \right)$$

$$= - \frac{N^2 \mu_0 \mu_r a}{l} \cdot \frac{di}{dt}$$

$$= -L \frac{di}{dt}$$

L = Inductance

$$= \frac{N^2 \mu_0 \mu_r a}{l}$$

Current induced in coil B due to change in current in coil A because of change in flux linkage

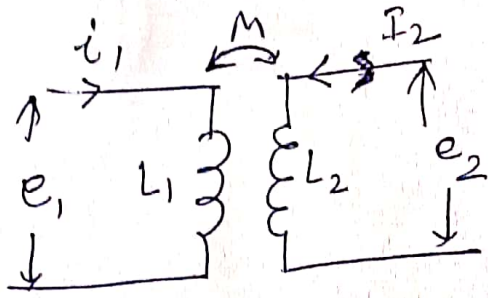
$$e_m = - \text{Rate of change of flux in coil B}$$

$$= -N_2 \cdot \text{rate of change of flux in coil A}$$

$$= -N_2 \cdot \frac{d}{dt} \left[\frac{N_1 i_1}{\mu/\mu_0 \mu_r a} \right]$$

$$= - \frac{N_1 N_2 \mu_0 \mu_r a}{l} \cdot \frac{di_1}{dt}$$

$$= -M_{12} \frac{di_1}{dt}$$



$$e_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$$

$$e_2 = L_2 \frac{di_2}{dt} + M \frac{di_1}{dt}$$

Coefficient of Coupling:

Flux in one coil links with the other coil, a fraction k . Let this factor be k .

Then $\phi_1 = \frac{N_1 i_1}{l / \mu_0 \mu_r a}$ Wb

Flux created by i_1 in N_1 turns.

Let this link by a factor k with coil 'B'

Then $\phi_2 = k \cdot \phi_1 = \frac{k N_1 i_1}{l / \mu_0 \mu_r a}$ Wb.

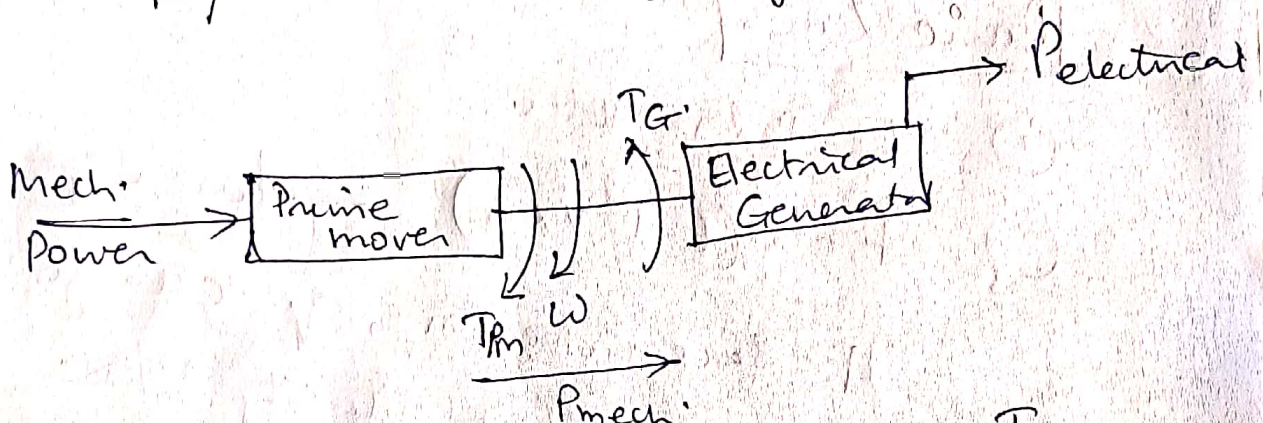
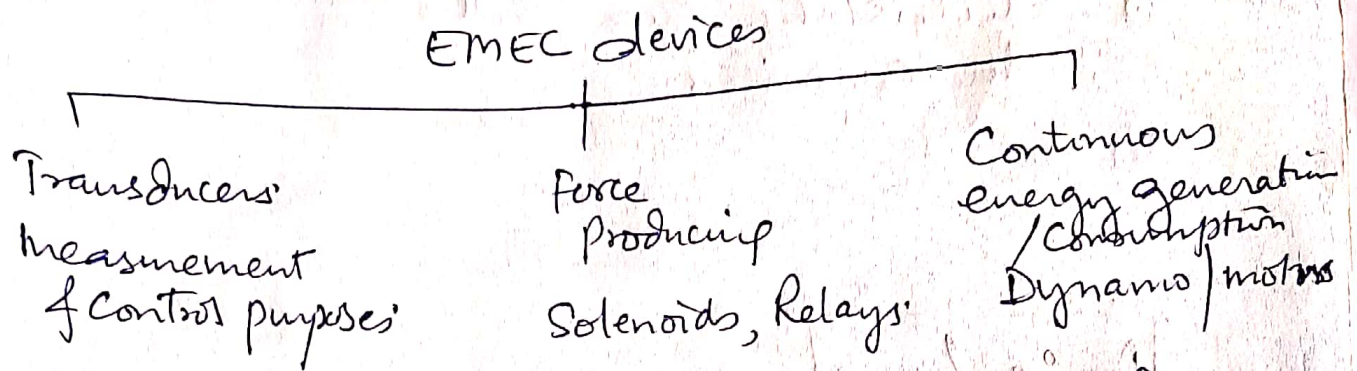
Mutual inductance $M_{12} = \frac{N_2 \phi_2}{i_1} = \frac{k N_1 N_2}{l / \mu_0 \mu_r a}$

Coefficient of self inductance $L_1 = \frac{N_1 \phi_1}{i_1} = \frac{N_1^2 \cdot i_1}{l / \mu_0 \mu_r a}$

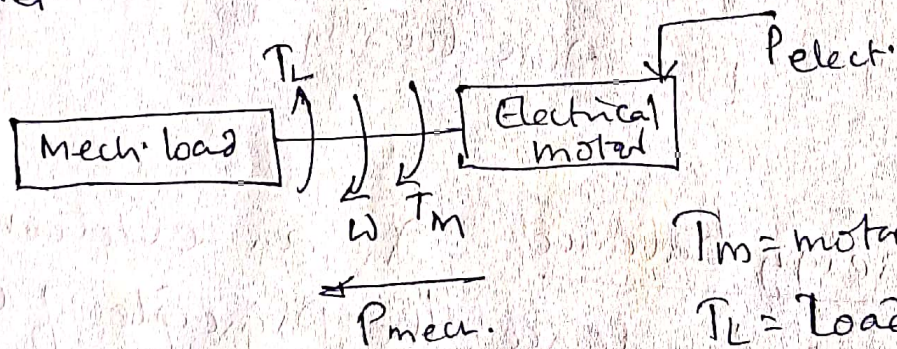
" " $L_2 = \frac{N_2^2 \cdot i_2}{l / \mu_0 \mu_r a}$

Principles of Electromechanical Energy Conversion (11)

EMEC



$T_{pm} \rightarrow$ Torque Prime mover
 $T_G \rightarrow$ Generator Torque
 $T_{pm} = T_G$



$T_m =$ motor torque
 $T_L =$ Load Torque
 $T_m = T_L$

EMEC device is a link between Electrical and mechanical systems.

All these devices make use of either or all

- 1) Force experienced on a Current carrying conductor in a magnetic field

- 2) Force of attraction or repulsion of a ferro-magnetic material
- 3) Electrostatic force on the charged plate of the capacitor
- 4)

Basic laws

① $E = Blv$ Volts.

② $F = q(E + v \times B)$ — Lorentz equation

F = force in Newton, q = charge in Coulombs

E = Electric field intensity V/m .

v = velocity of particle in m/s .

B = Flux density in Tesla.

Energy balance In an electromagnetic energy conversion device, the principle of Conservation of energy is applied between the stages of conversion.

Energy input from Electrical Source

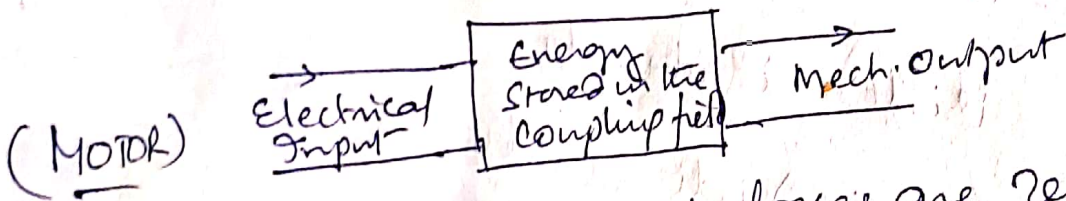
= Energy output in mechanical form + Energy converted to heat + increase in stored energy in magnetic field. (MOTOR active)

Similarly for Generator action

Mechanical Energy input

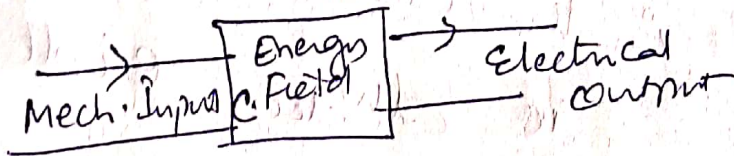
= Electrical energy Output + energy converted to heat + change in stored magnetic field.

Coupling Field Reaction

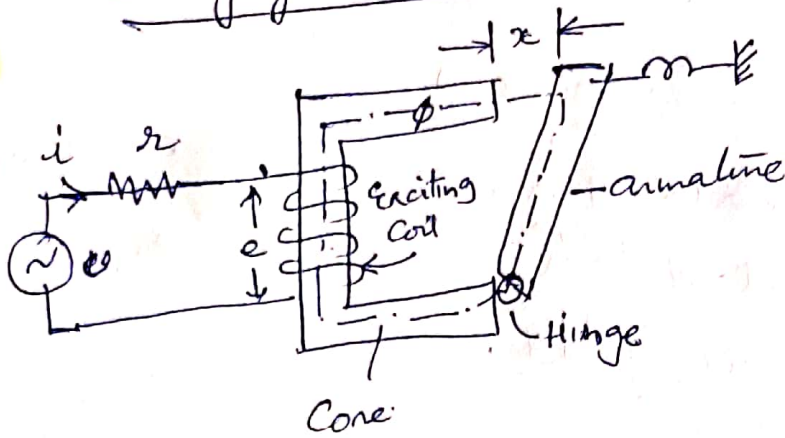


When the Coupling field losses are zero, i.e. the Coupling field is lossless then entire energy input is converted to proportional output.

(GENERATOR)



Singly excited Magnetic System



$$V = ir + e = ir + \frac{d\phi}{dt}$$

$$\text{or } Vi = i^2 r + ei = i^2 r + i \frac{d\phi}{dt}$$

$$\text{or } V i dt = i^2 r dt + i d\phi$$

$$\text{i.e. } (V - ir) i dt = i d\phi$$

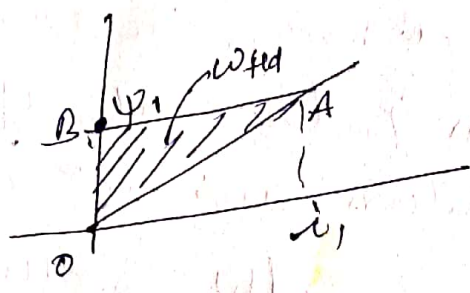
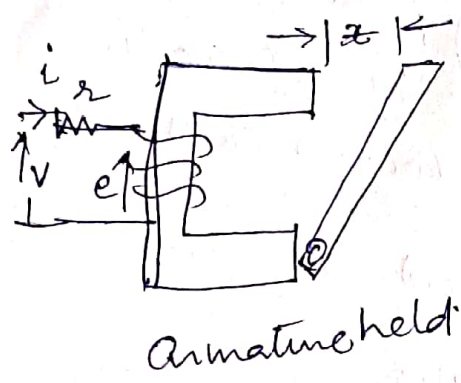
$$\text{or } \boxed{e i dt = i d\phi}$$

the electrical energy input to the coil is reflected in the change in flux linkages.

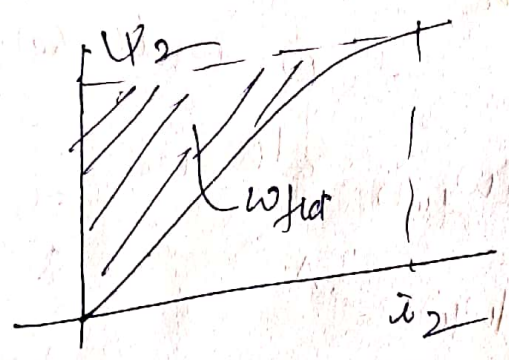
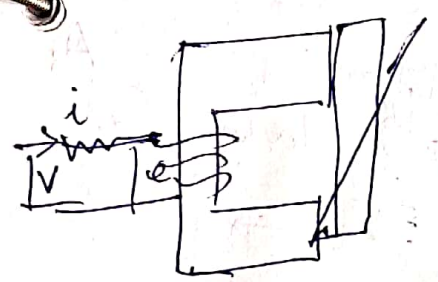
$$\text{i.e. } dW_{elec} = e i dt = i d\phi$$

In a toroidal core, all the flux links with the turns then $i d\phi = i N d\phi = (mmf) \cdot d\phi$

When mechanical work done



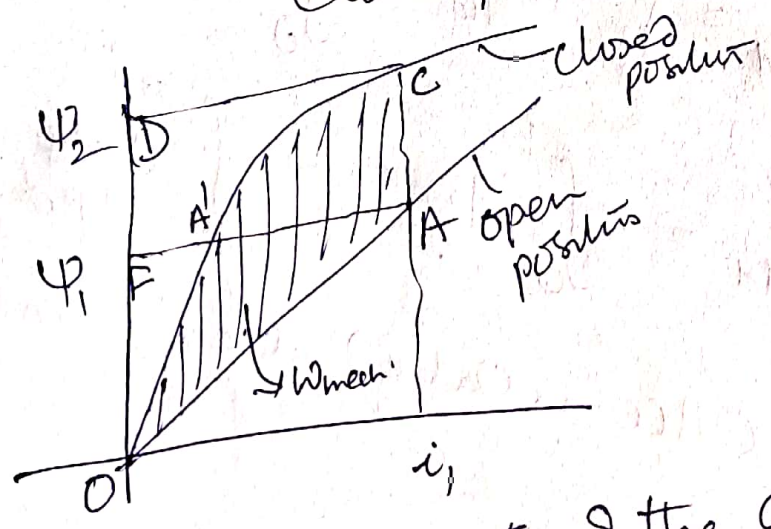
Armature held



$\phi_2 > \phi_1$

Slow movement

open position $\rightarrow \phi_1 \text{ \& } i_1$
 closed position $\rightarrow \phi_2 \text{ \& } i_2$

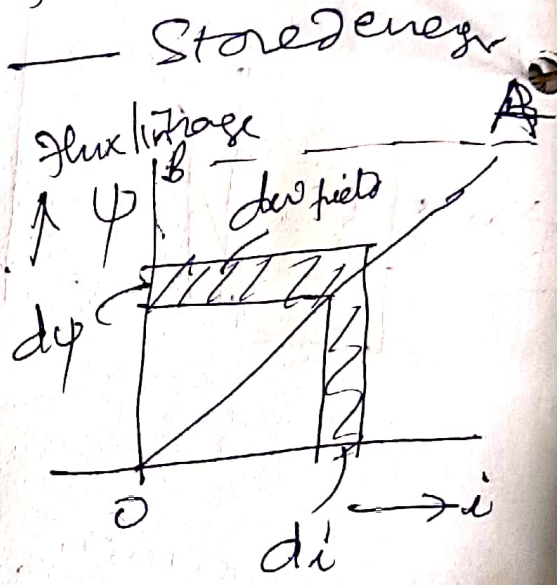
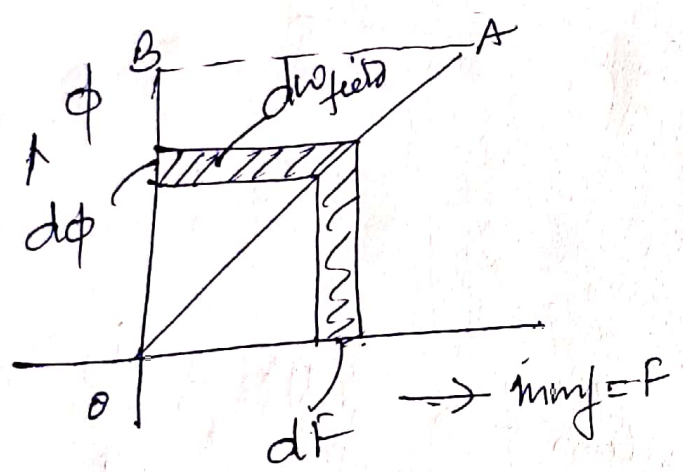


the slow movement of the armature is done such that the rate of change of flux linkages $\frac{\phi_2 - \phi_1}{\text{time}}$ is negligible

Magnetic field is stored, when the mechanical work done is zero. free in a magnetic relay, on the energisation of the coil, if armature is held in position and not allowed to move

then $dw_{elec} = dw_{work} + dw_{field}$
 $= 0 + dw_{field}$

or $dw_{field} = dw_{elec}$



$OABO = w_{fld} = \int_0^{\phi_1} dw_{fld} = \int_0^{\phi_1} F \cdot d\phi$

$OACO = \int dw'_{fld} = \int_0^{F_1} \phi dF = \int_0^{i_1} \phi di$

Area $OACO$ is called area of Co energy

Hence the operating point 'A' reaches 'E' along AC.

Change in stored energy from open to closed position

$$= W_{fld} = \text{Energy in closed} - \text{Energy in open position}$$

$$= \text{Area } OA'CDFO - OAA'FO$$

$$\text{Electrical energy input} = \int_{\psi_1}^{\psi_2} i d\psi = \text{Area } ACDA'A$$

$$\text{Since } W_{elec} = W_{fld} + W_{mech}$$

$$W_{mech} = W_{elec} - W_{fld}$$

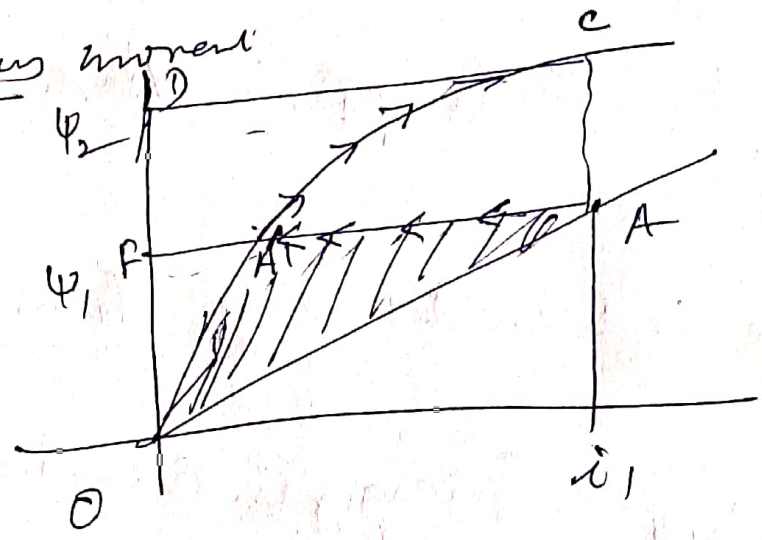
$$= ACDA'A - (OA'CDFO - OAA'FO)$$

$$= ACDA'A - OA'CDFO + OAA'FO$$

$$= \text{Area } OACAO$$

(Ignoring saturation, half of electrical input is stored as magnetic field and other as mech. output during slow motion of armature)

Instantaneous moment



for instantaneous moment ψ_1 is not changed
 the operating point travels from A to A' and
 from A' to c.

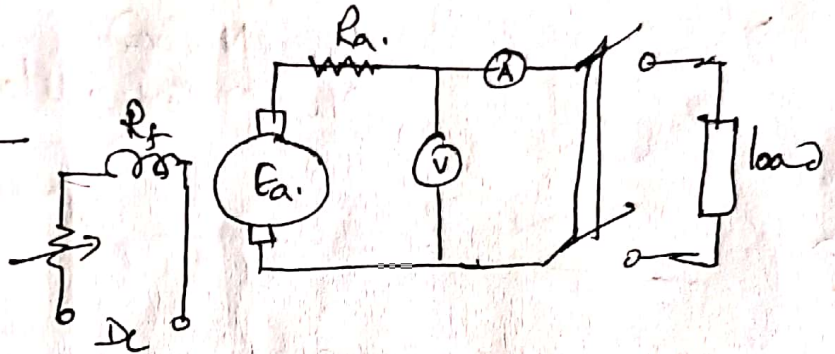
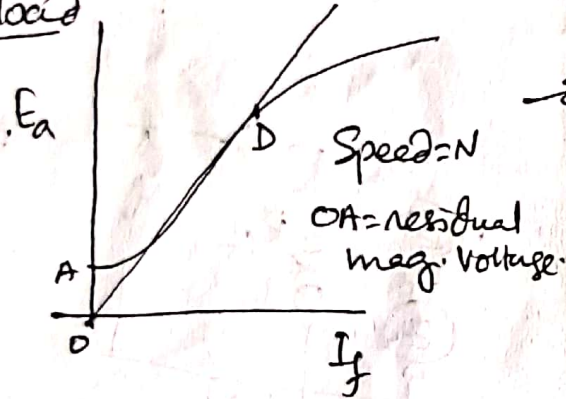
Shunt Generator

Characteristics

- ① Magnetizing characteristics or saturation w/open ct or no load } $E_a, V_s, I_f, N = \text{const}$
- ② Internal characteristics } $V_t, V_s, I_L : I_f \& N \text{ const}$
- ③ External characteristics } $V_t, V_s, I_f : I_a, N \text{ const}$
- ④ Load characteristics or load magnetization curve.

For Separately excited

① No load



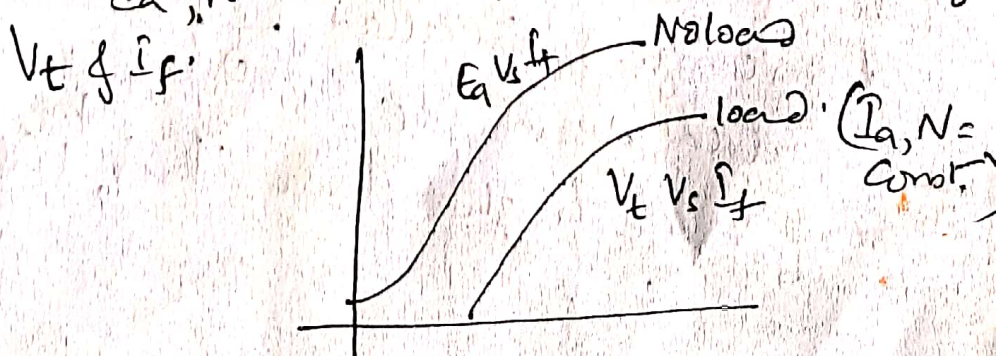
I_f is increased in steps till $E'_a = 1.1 E_a$.

If I_f is retraced, Curve plots is higher, because of hysteresis.

② load — V_t & I_f for $I_a, N \text{ const}$

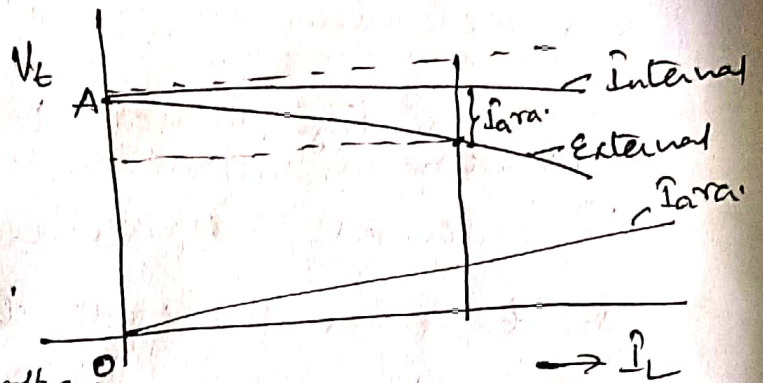
Adjust I_f to get rated arm. current I_a and maintain N constant.

Vary load and field current to maintain $I_a, N \text{ const}$. take the readings of V_t & I_f .



③ External V_t & I_L for $I_f, N = \text{Constant}$

Rated speed,
field winding adjusted to
give rated V_t .
load resistance is varied
and V_t and I_L noted.
OA = no load terminal voltage.

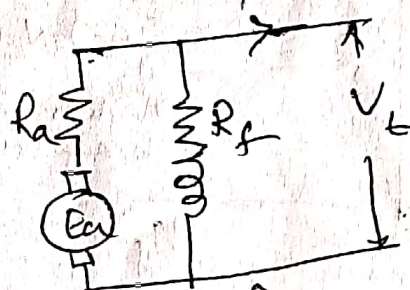


$$\text{Voltage regulation} = \frac{E_0 - V_n}{V_n} \times 100$$

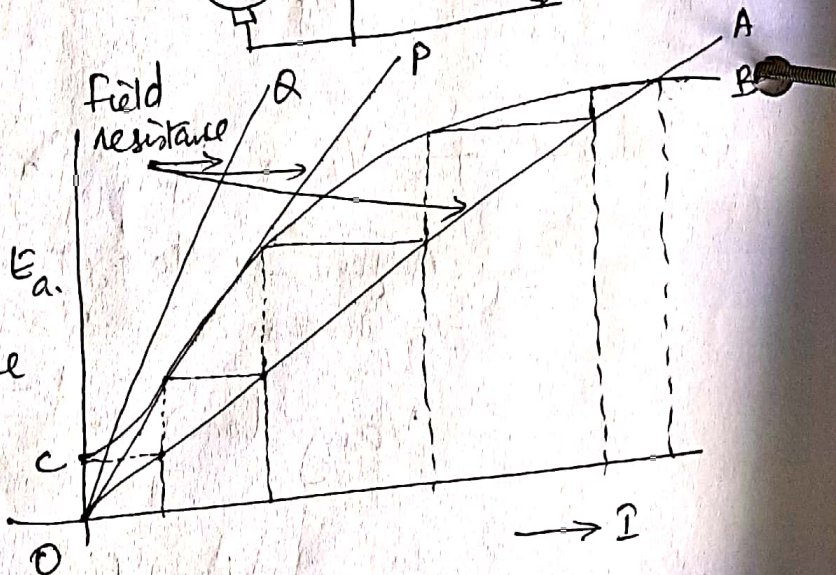
$E_0 =$ No load

$V_n =$ rated full load voltage.

Shunt generator



Voltage built up



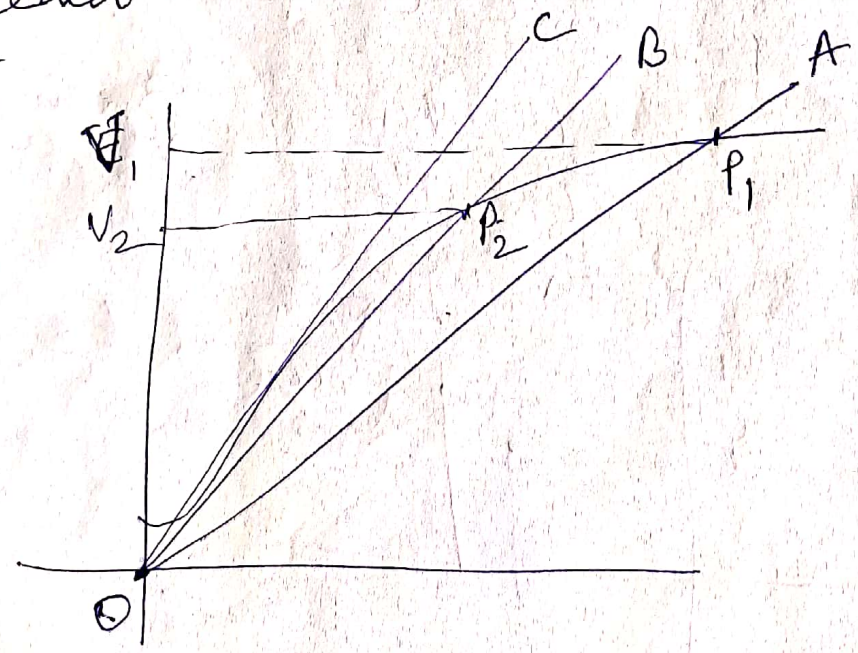
the value of field resistance
(line tangent to OQ curve
from origin) is called
Critical resistance.

Any value higher than this, will not generate.

Failure to build up voltage in a Shunt m/c.

- ① No residual magnetism. — excite field winding from a separate source.
- ② Field Connections are reversed.
- ③ High field resistance. → In this case the field resistance is greater than Critical resistance.
Reasons → open ckt in field, dirty commutator or large external resistance
- ④ Speed less than Critical speed. → Increase Prime mover speed.

OP represents the Critical field resistance R_c . $R_2 = OQ$ is greater than OP. Hence no built up voltage.



OA → field resistance R_1 , for which corresponding voltage is V_1 .
 OB is increased field R_2 , corresponding to V_2 .
 OC is R_3 for which ~~voltage is~~ V_1 .
 OP is called Critical res

Determination of

① Critical resistance from OCC

- a) Draw the OCC from data - induced emf and I_f .
- b) draw tangent from origin to OCC.
- c) Find the slope of the tangent to obtain critical resistance.

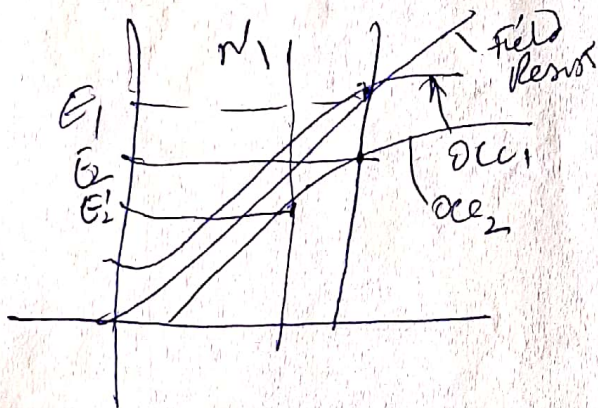
② OCC at different speed

a) plot OCC at given speed.

Since $E \propto \phi N$, or $E_1 \propto \phi_1$, $E_2 \propto \phi_2$

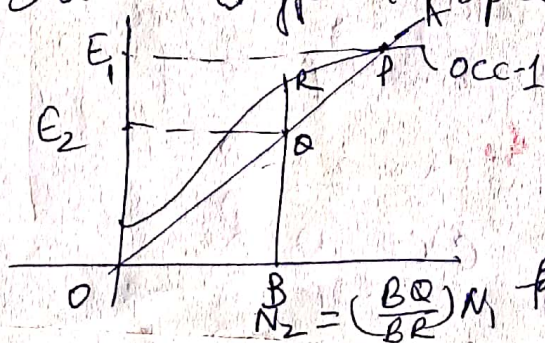
$$\text{or } \frac{E_1}{E_2} = \frac{N_1}{N_2}$$

Given any 3 values the other can be found



$$E_2 = \left(\frac{N_2}{N_1}\right) E_1$$

③ To obtain different speed for a given new emf.



Draw OCC-1
 Draw OA - field resist line
 P gives the operating point for E_1
 for any E_2
 or $N_2 = \left(\frac{E_2}{E_1}\right) N_1$

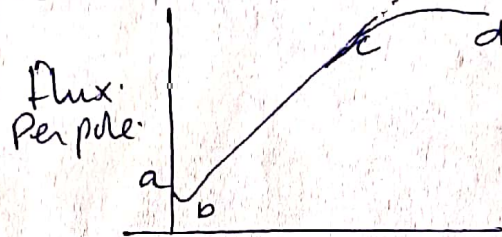
Operating Characteristics

1. Magnetization Curve.

$$E = \frac{\Phi Z N}{60} \cdot \frac{P}{A} \text{ volts.} = \left(\frac{Z P}{60 A} \right) (\Phi N) \text{ volts}$$

i.e. $E \propto \Phi N$ for a given m/c.

When speed is maintained constant, $E \propto \Phi$.



$E \propto \Phi \rightarrow N \text{ constant} \rightarrow \text{Field Ampereturns}$

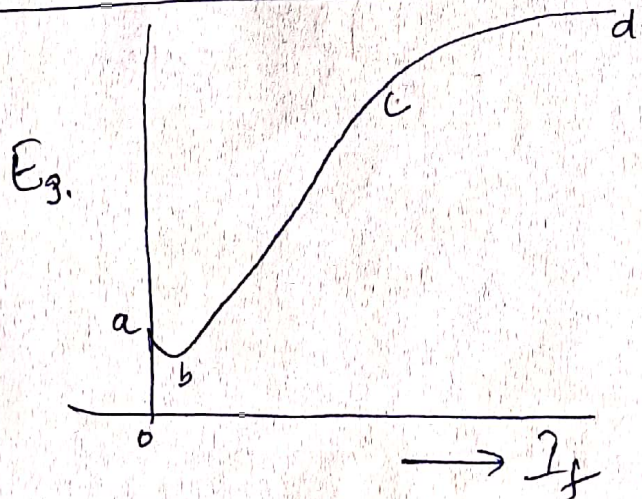
$\Phi \text{ (per pole)} \propto \text{Field ampere turns}$

$\propto I_f \cdot \text{Turns}$

$\therefore \Phi \text{ (per pole)} \propto I_f$ since Turns are fixed and hence constant

$\therefore E \propto I_f$

the graph between E & I_f is called the Open circuit Characteristics \rightarrow OCC or magnetic Characteristic

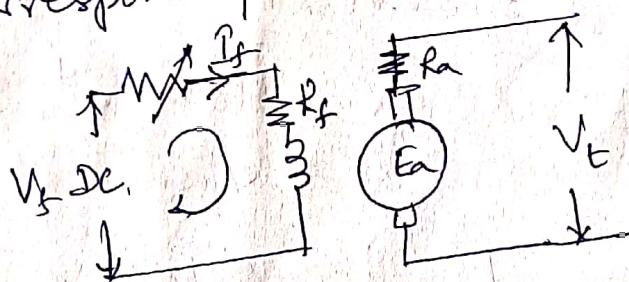


oa represents the residual magnetism.. 'bc' is the

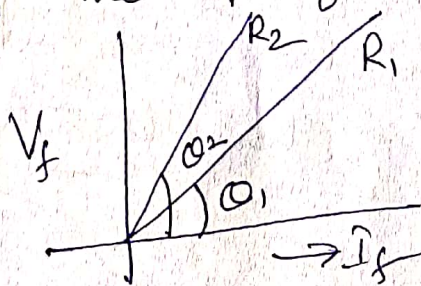
straight line portion and C the saturation starting point known as "knee" of the curve.

Experimentally determination:—

the field of series or shunt m/c is disconnected and connected through (A) of a source via a rheostat. m/c run at constant speed and on NOLOAD. Vary rheostat to get different readings of I_f and the corresponding E_a .



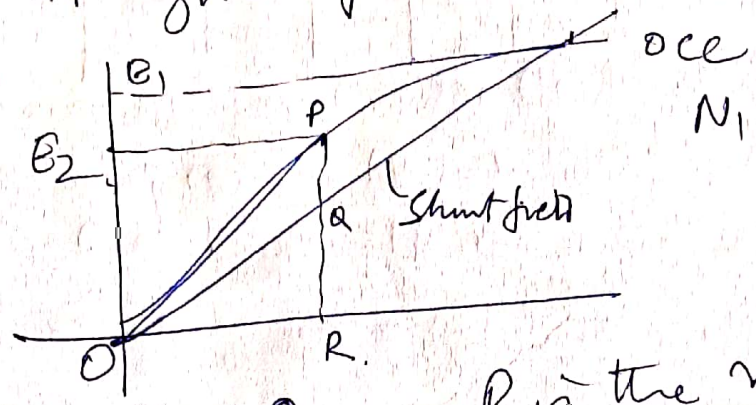
Field resistance line is a graph between V_f and I_f . The slope of the line $\frac{V_f}{I_f}$ gives R_f .



$$R_2 > R_1$$

$$O_2 > O_1$$

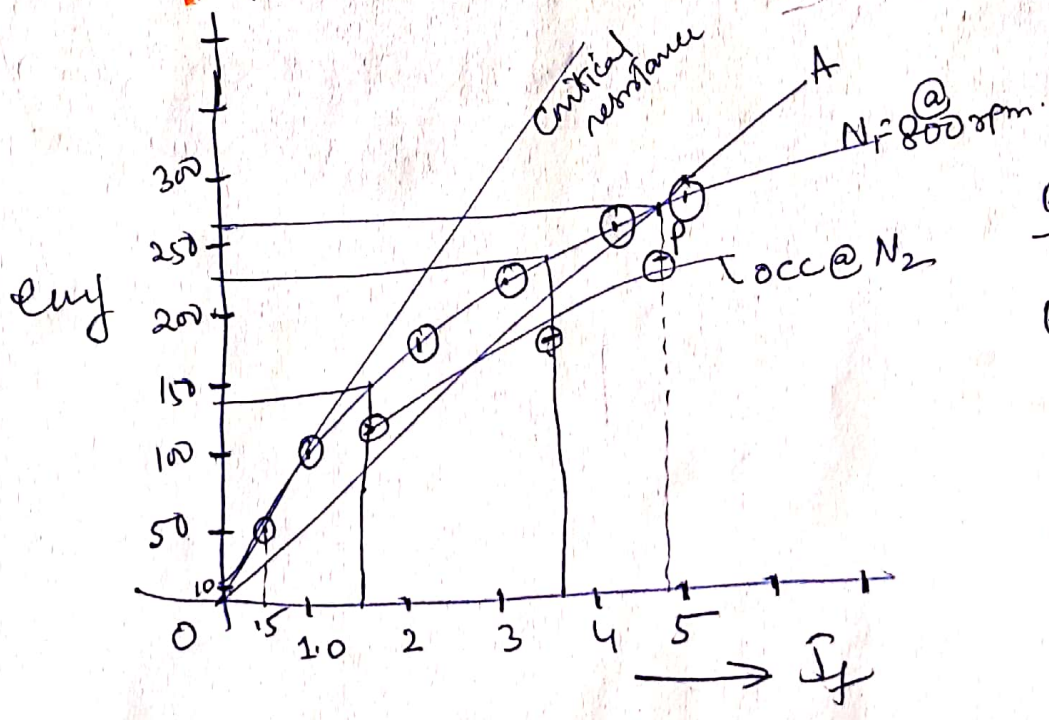
④ to reduce Shunt resistance, to obtain reduced E_{avg} at given speed



Corresponding to E_2 , P is the new operating point. the slope of OP is $\frac{PR}{OR}$ represents the new resistance of shunt field circuit

X

@ 800 rpm							
I_f	0	0.5	1.0	2.0	3.0	4.0	5.0
Induced E_{avg} (volts)	10	50	100	175	220	245	262



$$\frac{E_2}{E_1} = \frac{N_2}{N_1}$$

$$E_2 = \left(\frac{N_2}{N_1}\right) E_1$$

I_f	0	0.5	0.9	1.35	1.6	2.10	2.5	2.8	3.0	① 1500 rpm
E_b	7	65	140	180	210	233	245	265	275	

- find a) for a field resist 150Ω the no load emf
 b) the critical field at 1500 rpm
 c) the O.C. for 1150 rpm, and Critical resistance
 d) for ~~critical~~ ^{field} resistance of 100Ω the O.C. voltage.

4P, Shunt gen, Lap Connected $R_f = 50\Omega$ $R_a = 0.4\Omega$ Supply
 60ms 40W @ 100V. Calc I_a per path and efficiency,
 Assume 1V drop per brush

4P, Shunt, $R_f = 100\Omega$, $R_a = 1\Omega$, $Z = 378$, Wave Connected
 $\phi = 0.02$ wb, $R_L = 10\Omega$, $N = 1000$ rpm.
 Calc. power absorbed by load

4P, $\phi = 0.007$ wb, 400 Lap Conductors, each of resistance 0.002
 $N = 900$, $I_a = 50$ A Calculate V_t .

$$\left[\text{Arm resistance} = \frac{\text{Resist of conductors} \times (\text{no of Cond/path})}{\text{No of Parallel path}} \right]$$

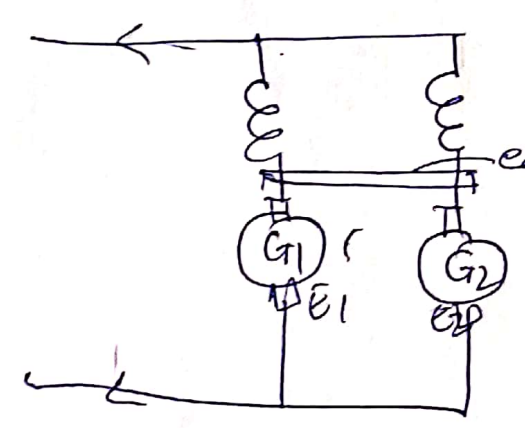
Voltage regulation % = $\frac{V_{NL} - V_{FL}}{V_{FL}} \times 100$

the field of shunt m/c or compound m/c should not be opened excepting when shunted through resistance called field break switch

Parallel operation of Gens

- Load fluctuates
- To supply varying loads, fixed value generator is not economical and efficient.
- To increase reliability
- to take care of maintenance/repair
- power plant can be augmented.

Parallel operation of Series Gens



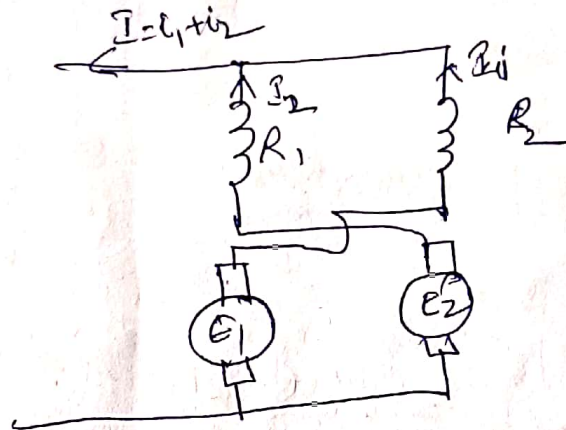
Two m/c of resistance R_{G1} & R_{G2} .
 equalizer bar for $E_1 = E_2 \rightarrow$ load shared is equal
 in case $E_1 > E_2$, circulating currents will flow $\frac{E_1 - E_2}{2r} = i$
 Current = $I + i$ and $I - i$.

↑ I, causes ↑ E_1 thereby increasing
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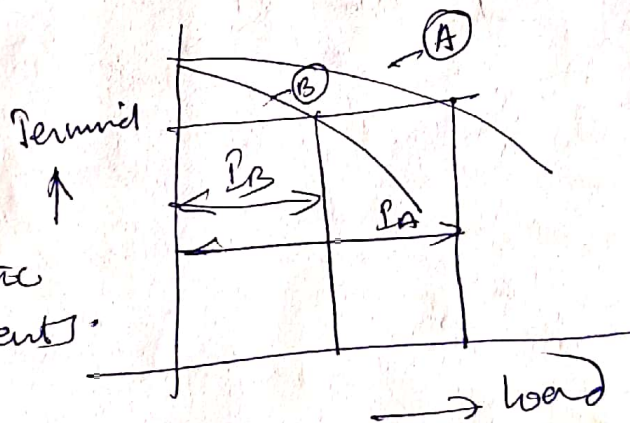
(10)

a stage will come when E_2 reverses its direction
 hence $E_1 - (-E_2) = E_1 + E_2$ is the net voltage.
 the current would be $\frac{E_1 + E_2}{2R} \Rightarrow$ high current
 nearly short circuit
 hence equalizer bar is connected

alternative arrangement \Rightarrow Cross Connect



Shunt gap
 Generated with more
 drooping characteristic
 carries lesser current.



Conditions

- ① Same polarity
- ② Equal terminal voltage
- ③